

# Best milling practices in feeding, extraction and power consumption

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Queensland University of Technology

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# Overview of presentation

- Three topics
  - Feeding
  - Extraction
  - Power consumption
- Focus on individual milling units
  - Extraction in particular is also considerably affected by cane preparation and added water rate

# Feeding



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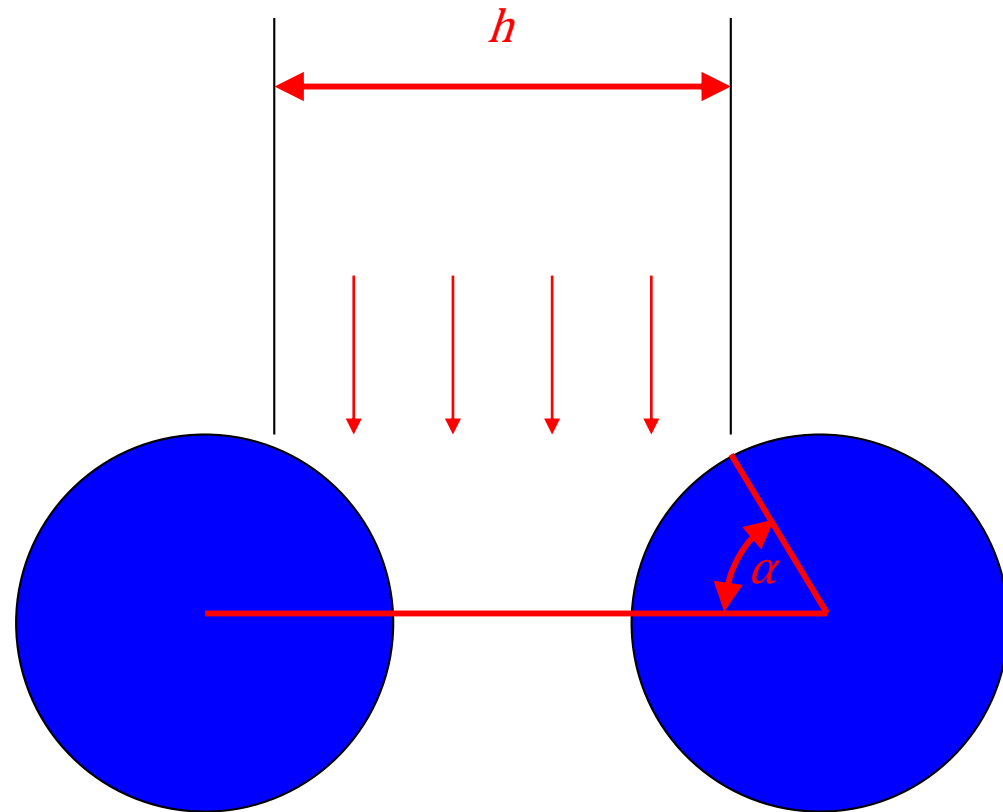


# Feeding

- Definition
  - The cane or cane fibre rate that can be achieved at a particular mill speed
- Associated with the capacity of the mill

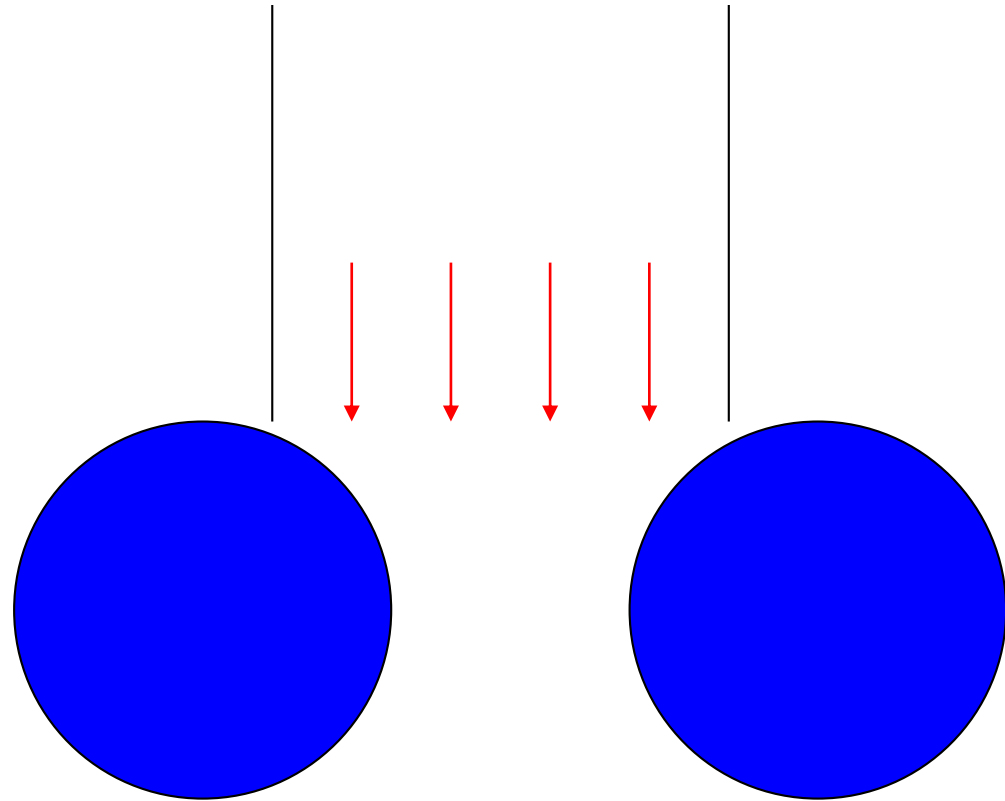
# Basis for feeding theory

- Based on two-roll mill
- Compaction ( $\gamma$ ) at Donnelly chute exit:
$$\gamma = \frac{Q_f}{LhS \cos \alpha}$$
- $Q_f$  Cane fibre rate
- $L$  Roll length
- $h$  Chute setting
- $S$  Roll surface speed
- $\alpha$  Contact angle



# Compaction at Donnelly chute exit

- Compaction at chute exit not affected by mill settings
- Function only of conditions in chute
- Essentially constant year to year



# Predicting mill speed

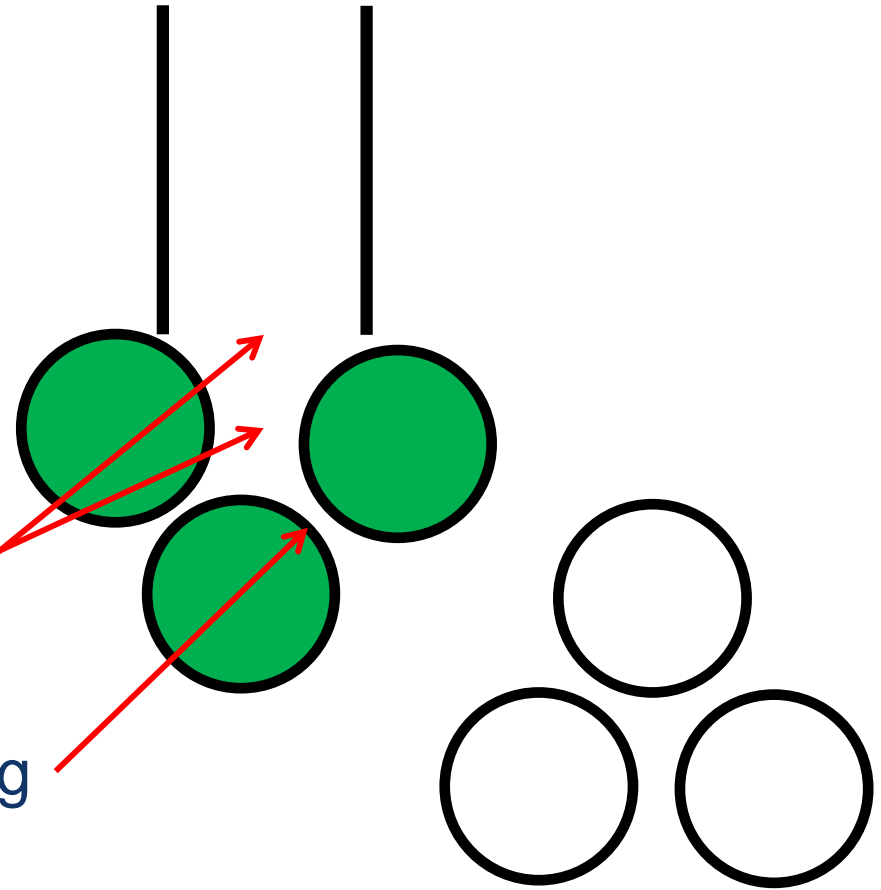
- Assumption of constant compaction at Donnelly chute exit can be used to predict mill speed
- Rearranging the compaction equation:

$$\gamma = \frac{Q_f}{LhS \cos \alpha} \Rightarrow S = \frac{Q_f}{\gamma Lh \cos \alpha}$$

- Compaction ( $\gamma$ ) from previous performance
- Roll length ( $L$ ), chute setting ( $h$ ) and contact angle ( $\alpha$ ) from mill geometry
- Fibre rate ( $Q_f$ ) selected

# Application of the feeding theory concept

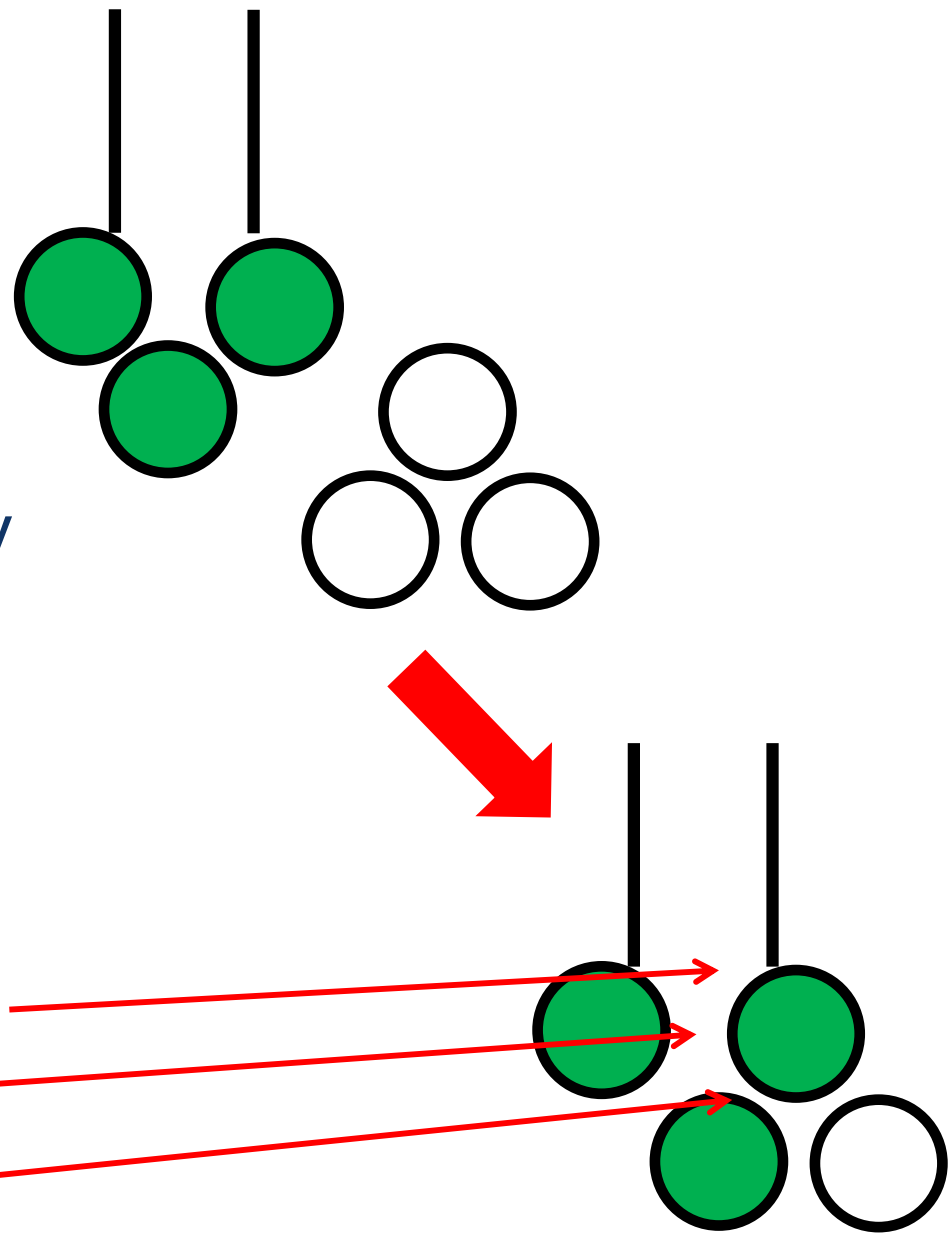
- As originally conceived, the theory was applied to the pressure feeder
- Theory indicates that mill speed is affected by:
  - Donnelly chute exit setting
  - Underfeed setting
  - Pressure feeder work opening





# Application to four-roll mill

- Pressure feeder geometry very similar to first three rolls in four-roll mill
- Theory indicates that mill speed is affected by:
  - Donnelly chute exit setting
  - Underfeed setting
  - Feed work opening



# Implications

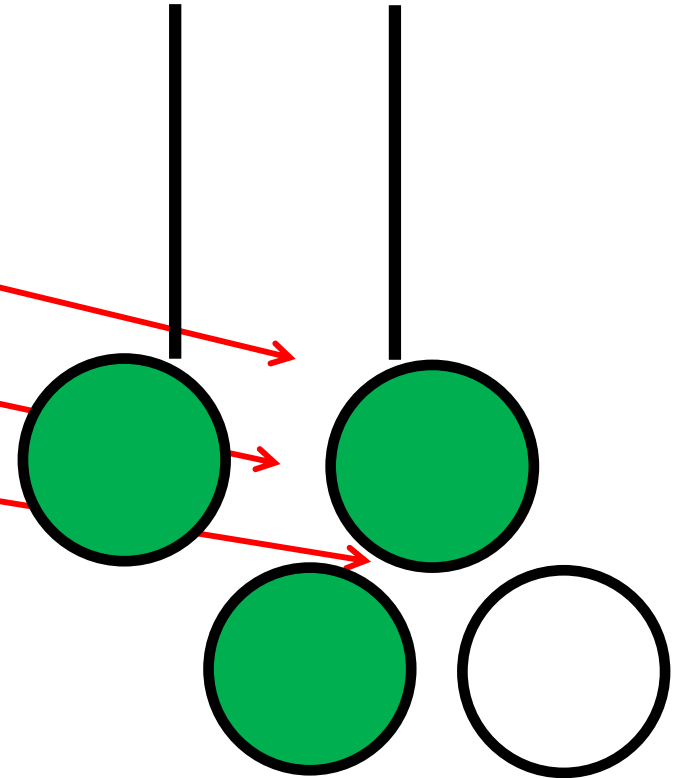
- Choice of settings will affect mill speed
- If the mill is operating near the middle of its speed range, there are no consequences
- If the mill is operating near the top or bottom of its speed range, chute height cannot be properly maintained
- Feeding theory can be used to adjust settings so mill operates in a better speed range

# Best practices in feeding

- Setting selection
- Roll surface grip and drainage

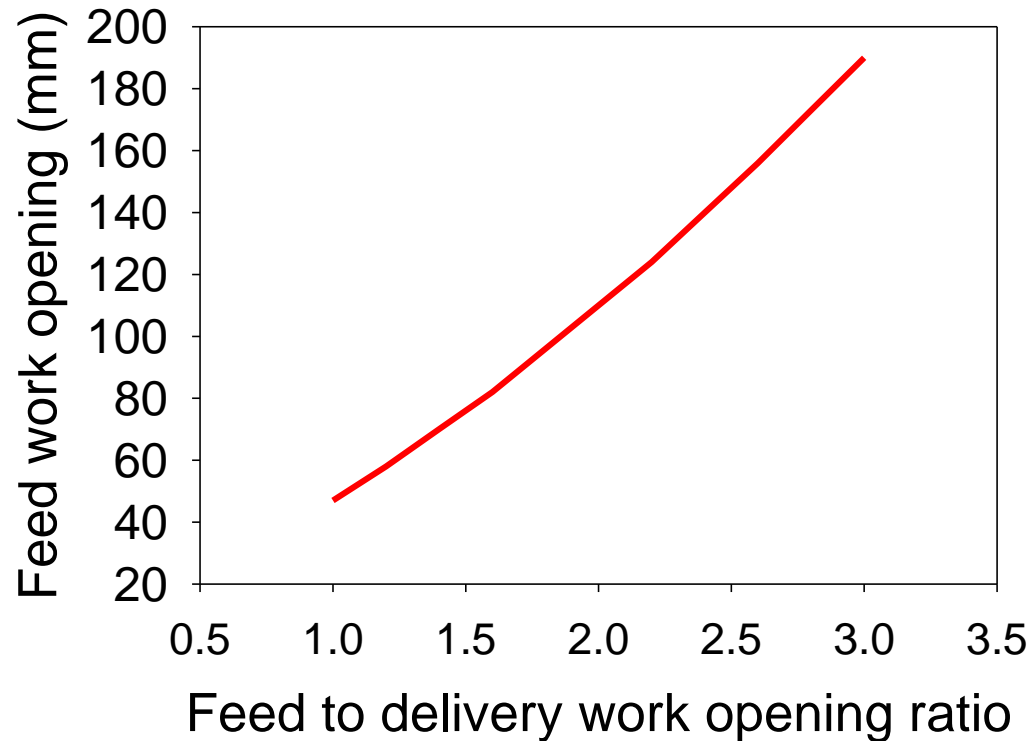
# Setting selection

- Choice of settings affects speed:
  - Donnelly chute exit
  - Underfeed nip
  - Feed nip
- Case study for a dewatering mill at Sezela (South Africa) reported SASTA 2014



# Effect of mill ratio on feed work opening

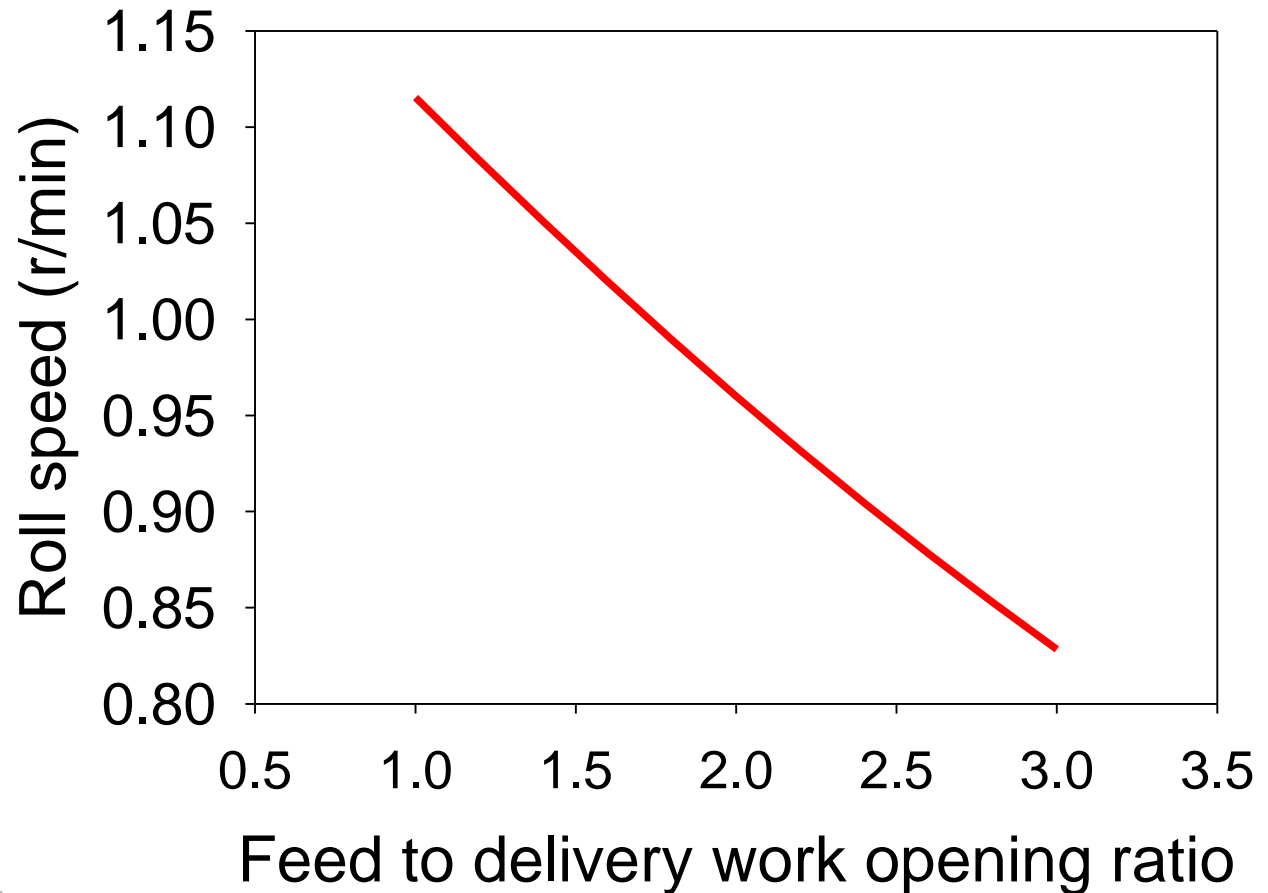
- Mill ratio is ratio of work openings between feed and delivery nips
- Typically used to calculate feed setting
- As set:
  - Work opening ratio 1.8
  - Feed work opening 93 mm



# Effect of mill ratio on roll speed

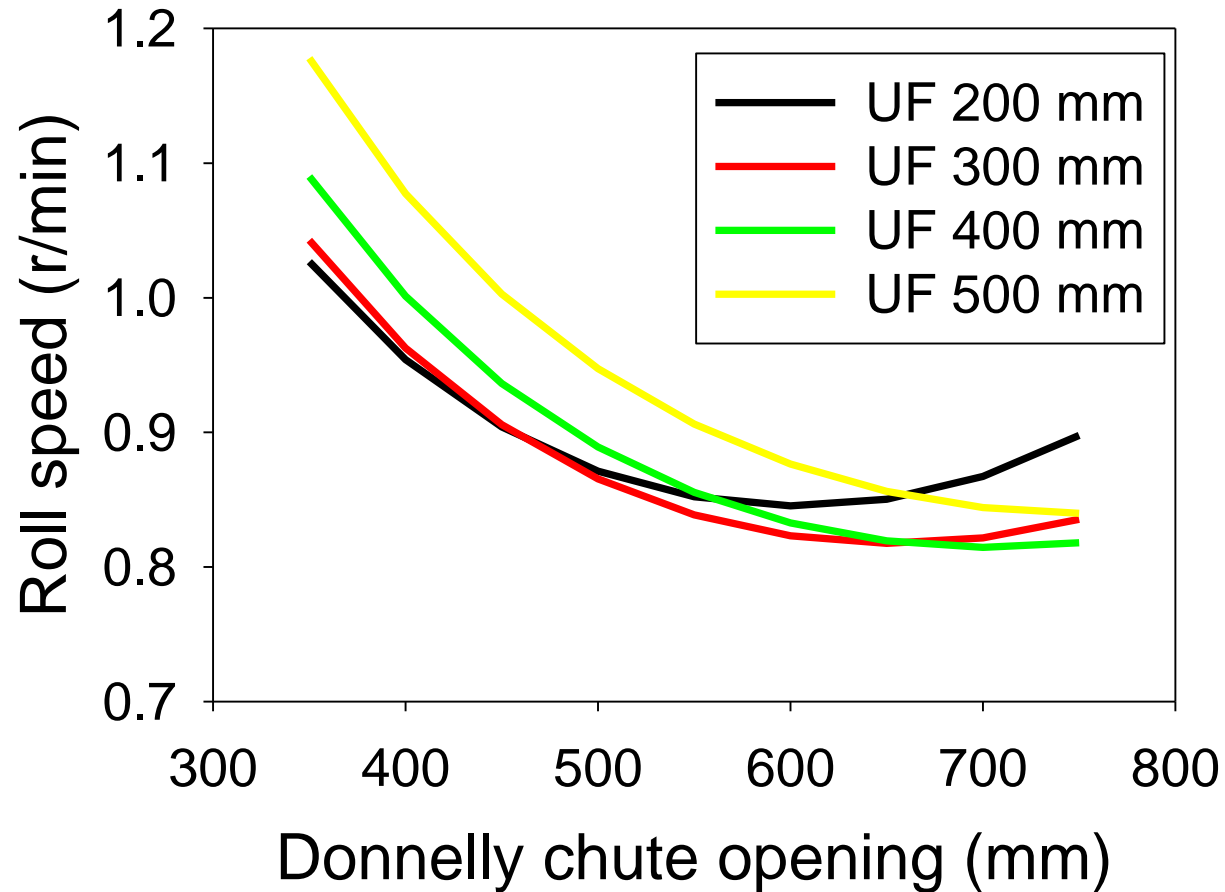
- As set:

- Work opening ratio 1.8
- Speed 1.0 r/min



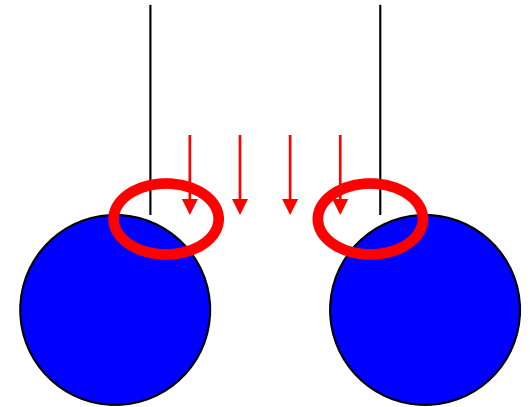
# Effect of underfeed and Donnelly chute exit opening

- Feed work opening 93 mm
- As set:
  - UF 216 mm
  - Donnelly 369 mm



# Roll surface grip

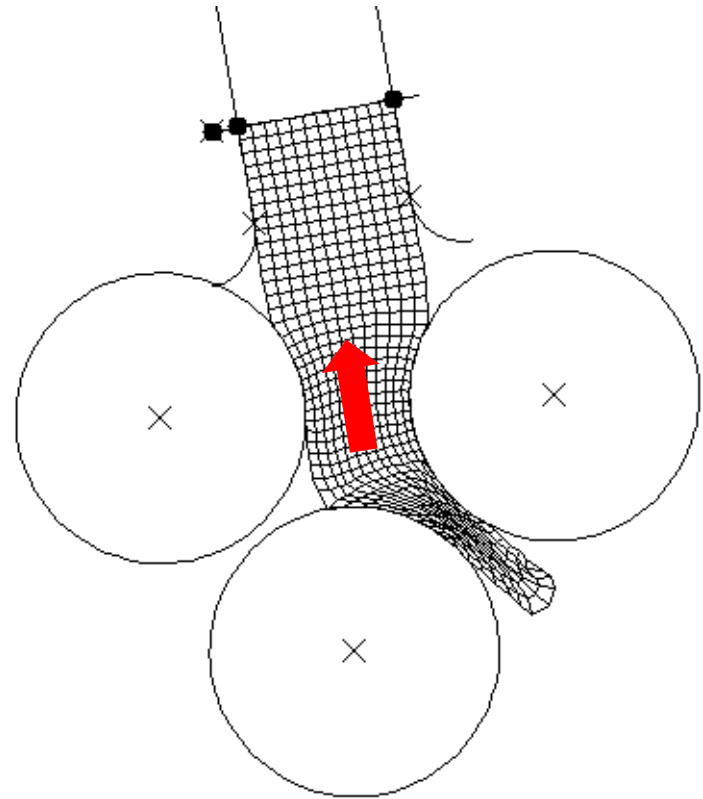
- Feeding dependent on rolls gripping the bagasse
- Picots seem a good way of doing that





# Roll surface drainage

- If juice cannot easily drain away from the roll surface, it has to force its way back in the direction of feeding
- Bad for feeding
- Solutions
  - Messchaert grooves
  - Lotus rolls



# Extraction



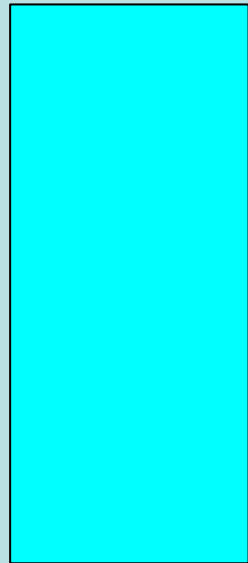
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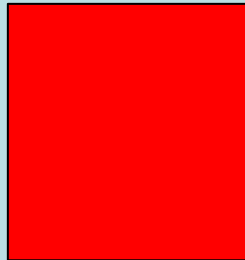
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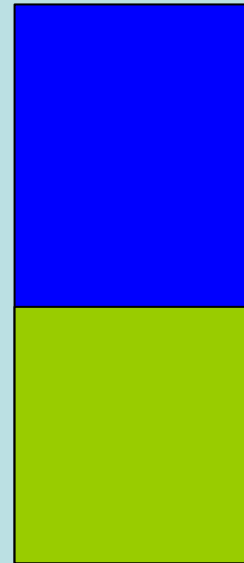
# Volumetric theory of juice extraction



Feed to  
mill



Expressed  
volume

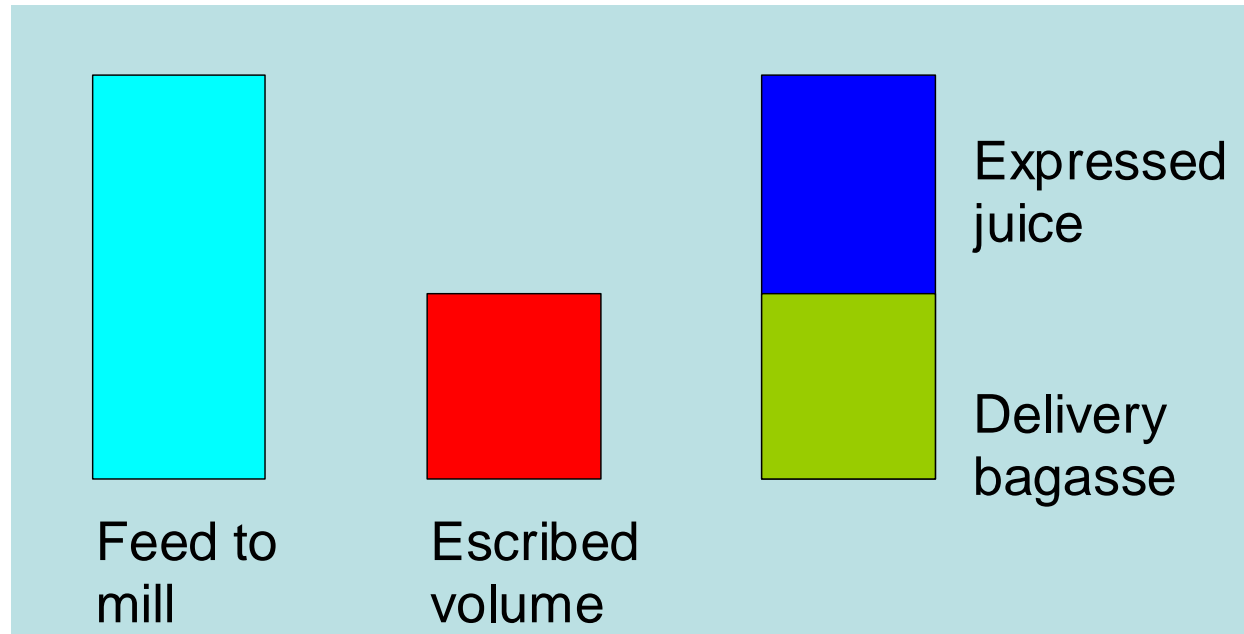


Expressed  
juice

Delivery  
bagasse

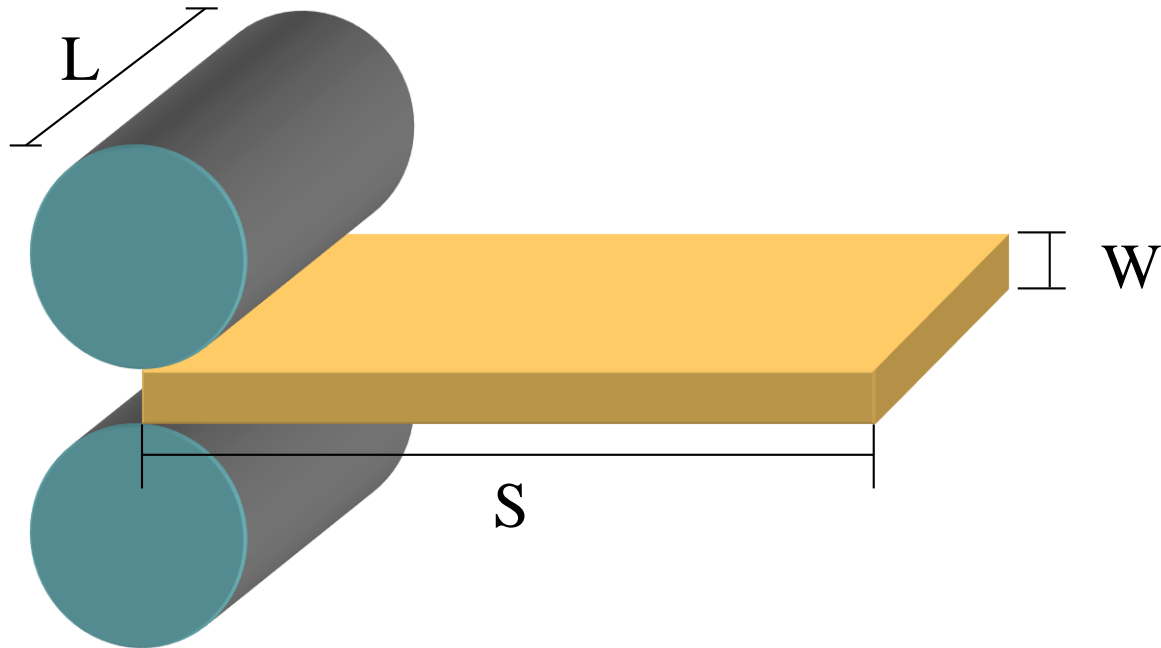
# Increasing extraction approach 1

- Volumetric theory shows that reducing escribed volume will reduce volume of delivery bagasse
  - Hence increase extraction



# Escribed volume ( $V_E$ )

- Escribed volume of final nip influences extraction
- $V_E = LWS$
- $L$  = roll length
- $W$  = work opening
- $S$  = surface speed



# Influencing escribed volume

- Option 1: change top roll hydraulic pressure
- Increases delivery nip compaction
- If increasing pressure, need to ensure top roll shaft has sufficient strength



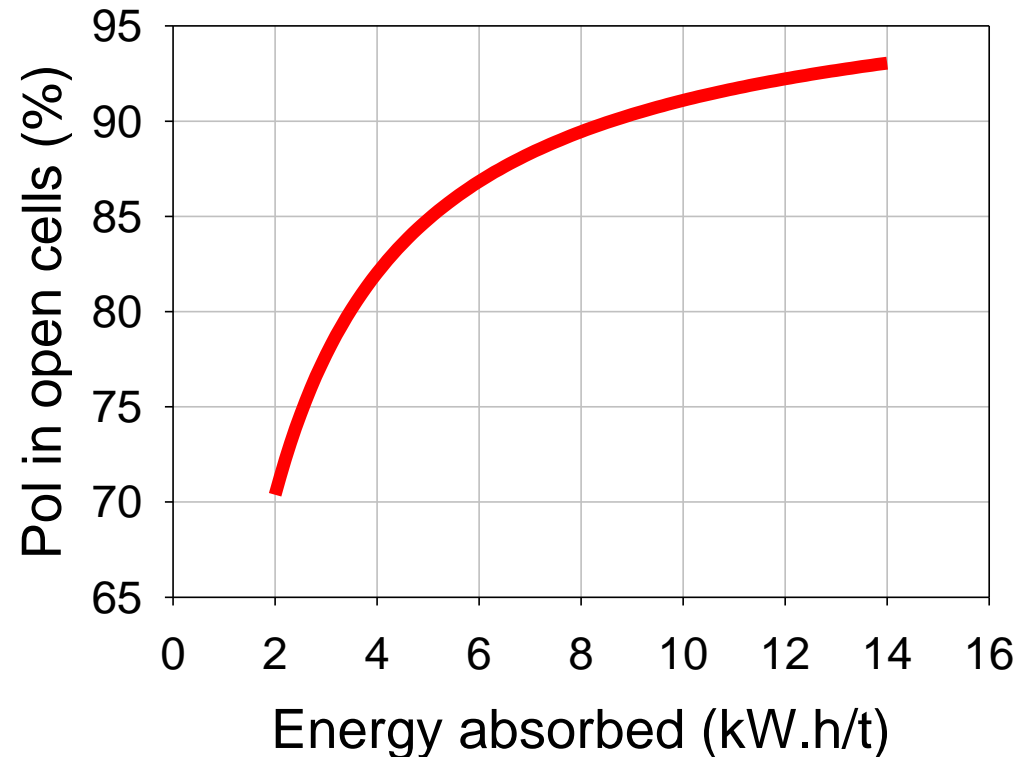
# Influencing escribed volume

- Option 2: enable higher delivery nip compaction at the same hydraulic pressure
  - Better preparation
  - Softer bagasse



# How to change bagasse preparation?

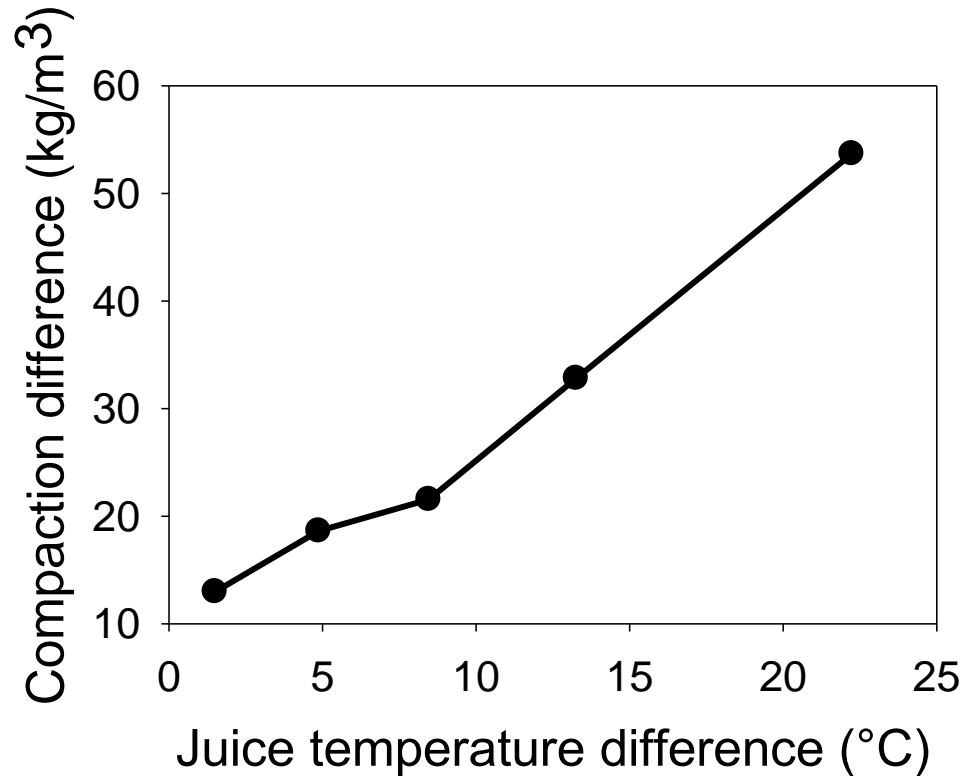
- Change cane preparation
  - Change power consumption
- Change preparation in mills
  - Increase hydraulic pressure in earlier mills



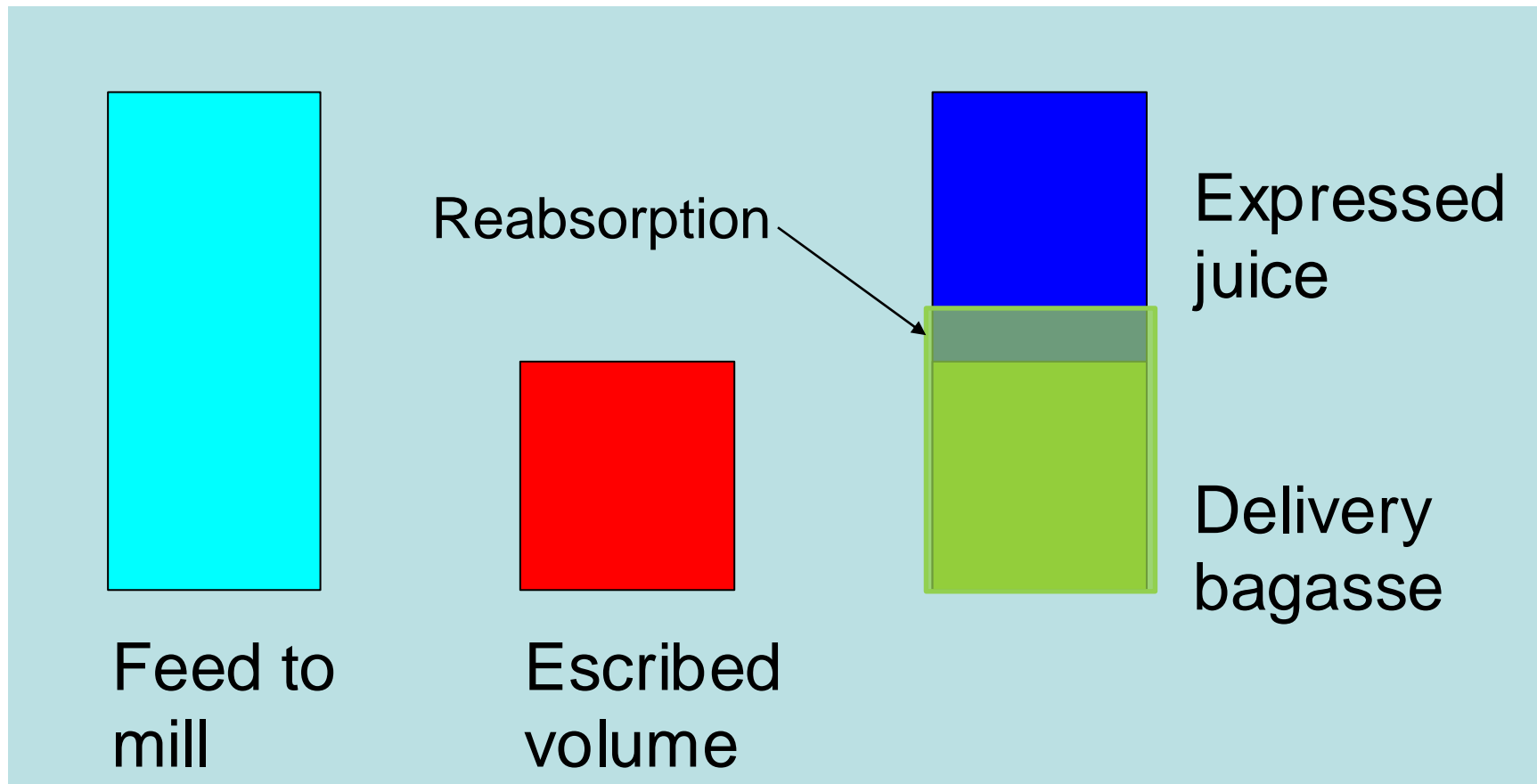


# How to change bagasse softness?

- Change added water temperature
- Higher temperature softens the fibres

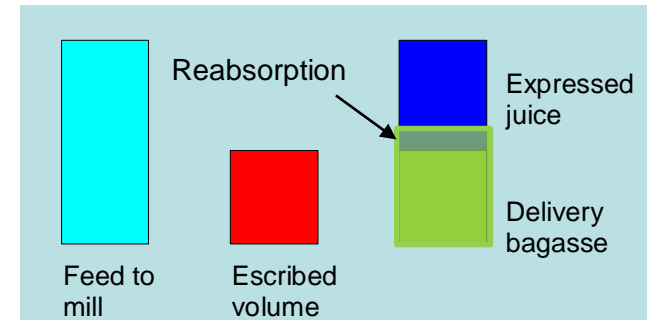


# The real extraction process



# Increasing extraction approach 2

- Based on volumetric theory
- Reduce reabsorption factor ( $k$ )
- Volume of bagasse (based on fibre rate and delivery bagasse constituents) larger than escribed volume



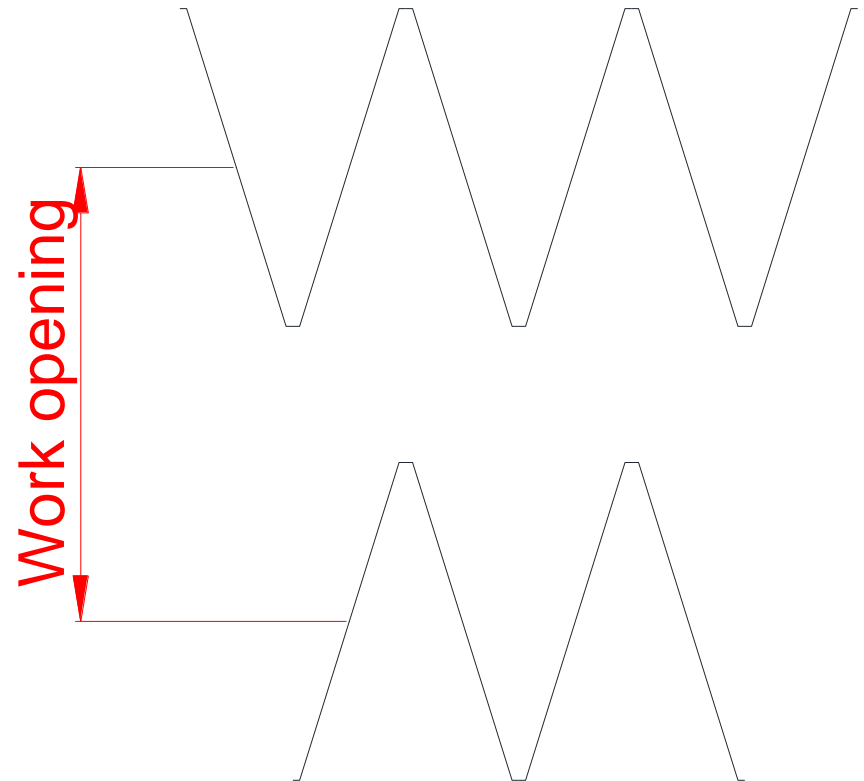
$$k = \frac{V_B}{V_E}$$

# Understanding reabsorption

- Strongly dependent on definition of escribed volume
  - Definition of work opening  $W$
  - Definition of surface speed  $S$

# Definition of work opening

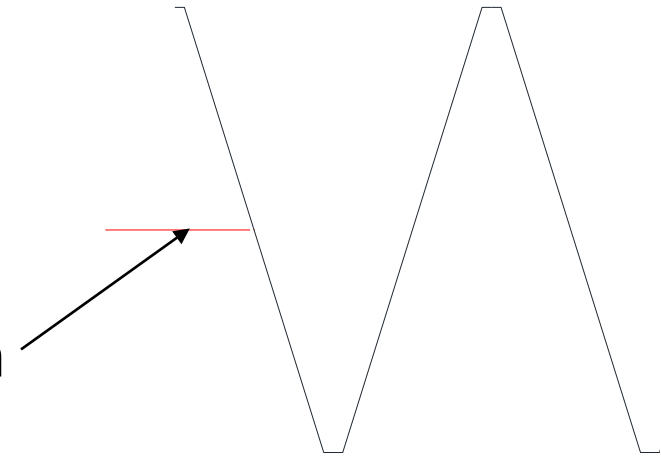
- Defined half way into grooves
- Assumes:
  - Tip area inside work opening space where bagasse cannot fill is same as groove area outside work opening space where bagasse can fill
  - Groove is filled with bagasse



# Definition of surface speed

- Also defined half way into grooves
- Defined for top roll only

Surface speed definition



# For reabsorption to occur...

- Need to have more bagasse passing through nip than indicated by escribed volume definition
  - Consider fibre and juice

# Possible mechanisms of reabsorption

- Juice flowing forward through or around grooves
- Bagasse slipping forward between rolls
  - Insufficient roll roughness to grip bagasse
- Bagasse extruding forward due to internal shear



# Juice flow over rolls

- Particular problem for four-roll mills



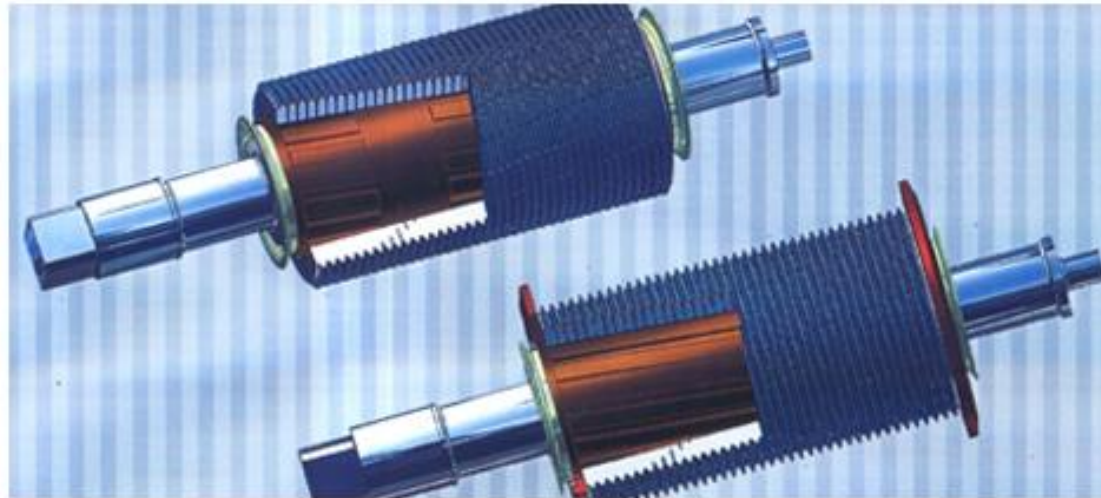
# Juice suction system

- Option to extract juice from behind the top roll before it flows over the top
- Four-roll mill experiment found juice suction reduced reabsorption factor by 5%



# Lotus rolls

- Significant increase in popularity in last few years
- Ability to draw in juice and prevent it from flowing over top roll
- Good option for four-roll mills

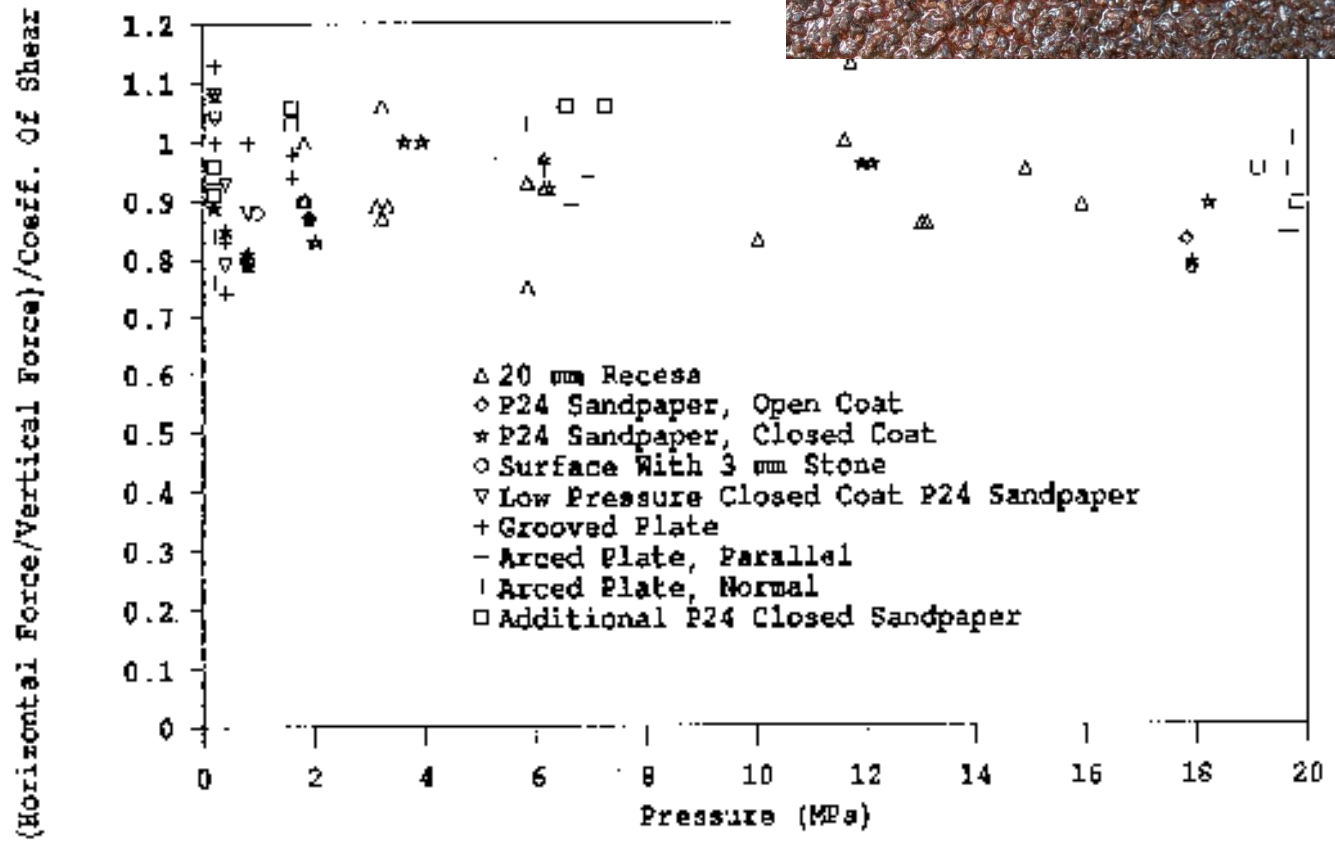




# Bagasse slipping forward

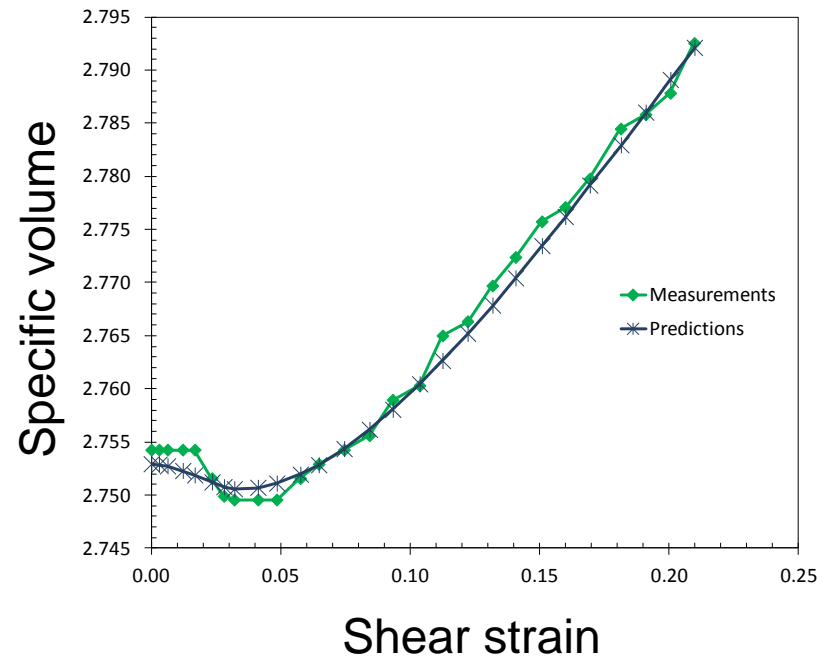
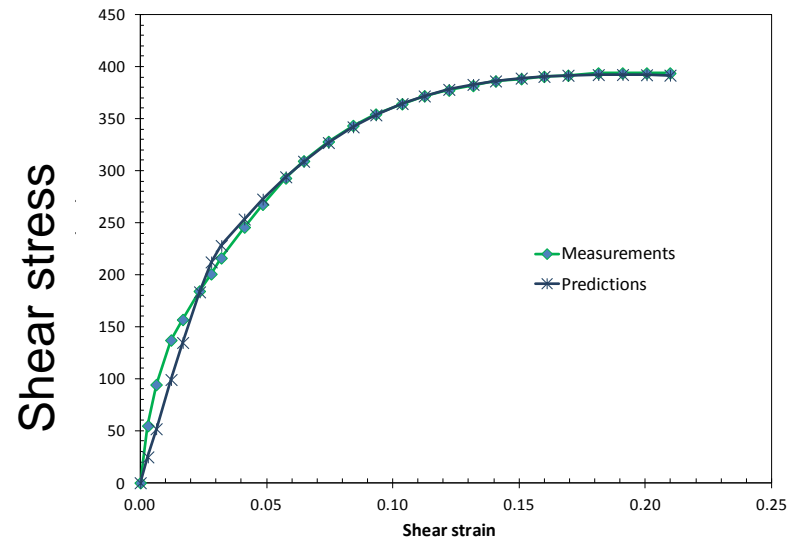


Tests have shown that a rough sandpaper (P24) is sufficient for bagasse to grip



# Bagasse shearing

- Stress/strain behaviour of bagasse is complex
- Finite element analysis modelling has provided some insights of stress states of bagasse in mills



# Other methods of controlling reabsorption

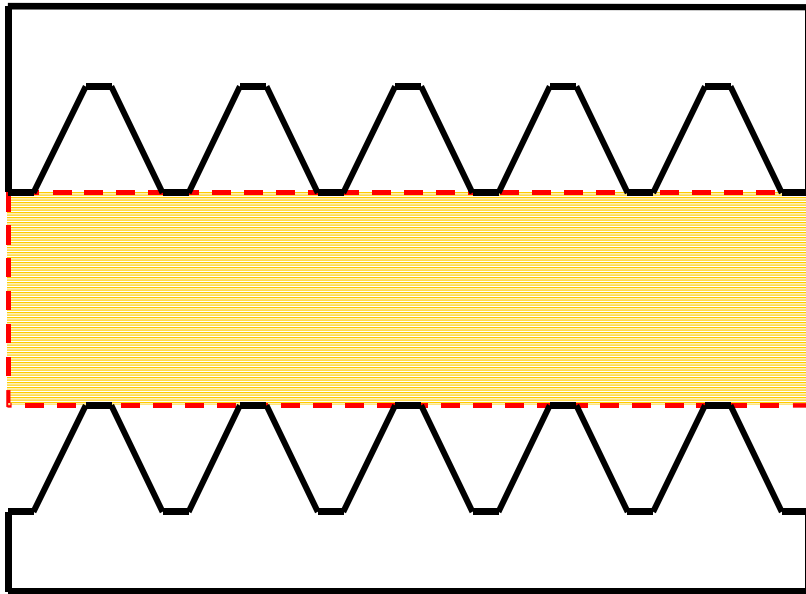
- There are few conclusive methods for reducing reabsorption
- Some options that may help
  - Groove profile
  - Roll roughness
  - Mill ratio
  - Trash plate design and setting
  - Mill control

# Groove profile

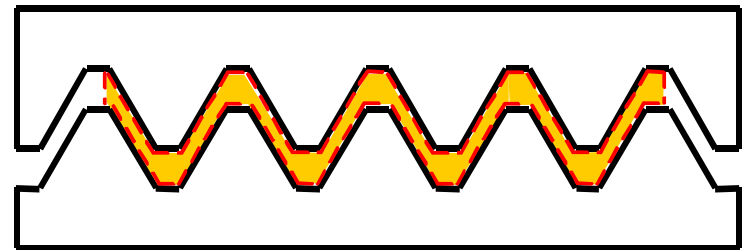
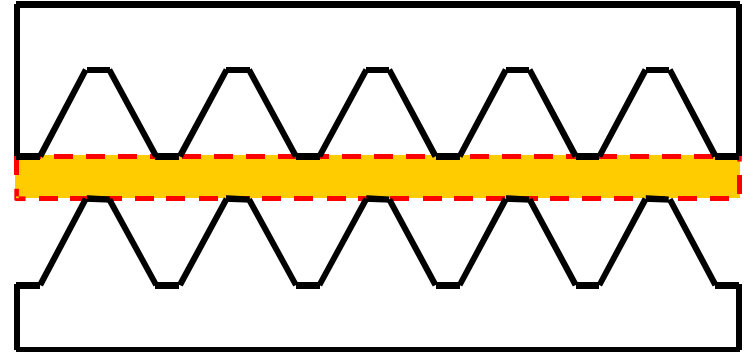
- Conducted compression tests with a range of groove profiles
  - Pitch
  - Angle
- Better extraction with
  - Higher pressure
  - Larger sample (work opening)
  - Wider angle



# Why may wider grooves be better?



Initial state



Possible final states



# Roll roughness

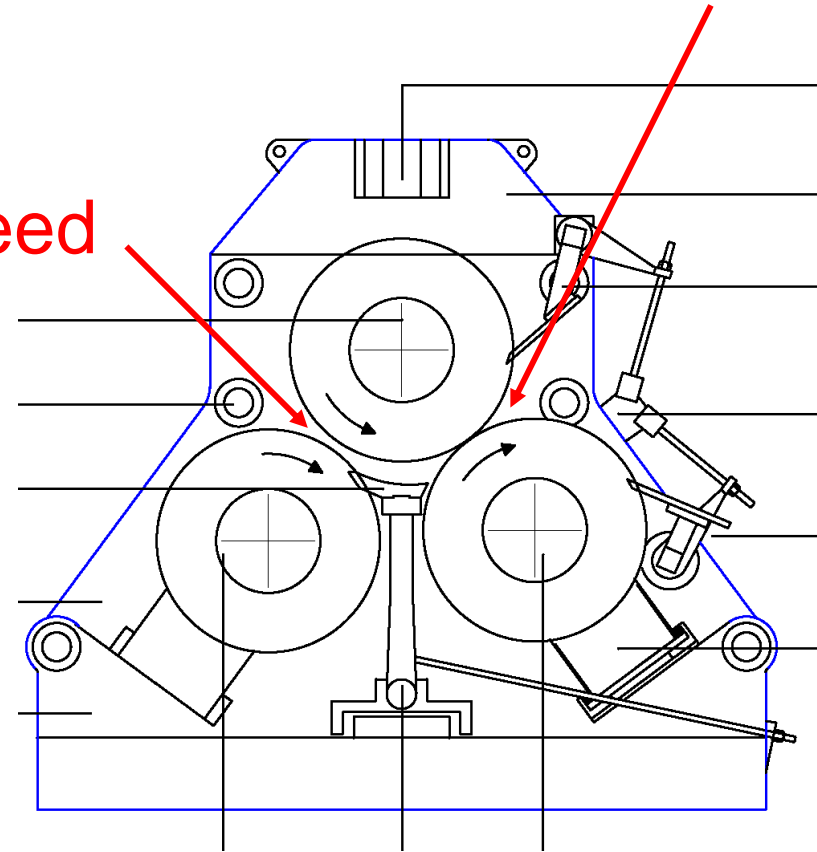
- One Australian sugar factory used to use reabsorption factor measurements to determine when to arc rolls



# Mill ratio

Delivery

Feed



- Ratio of escribed volumes of feed to delivery
- Low mill ratio expresses more juice in feed nip so cannot be reabsorbed in delivery nip
- Low mill ratio reduces load that can be applied at delivery nip and so reduces delivery escribed volume

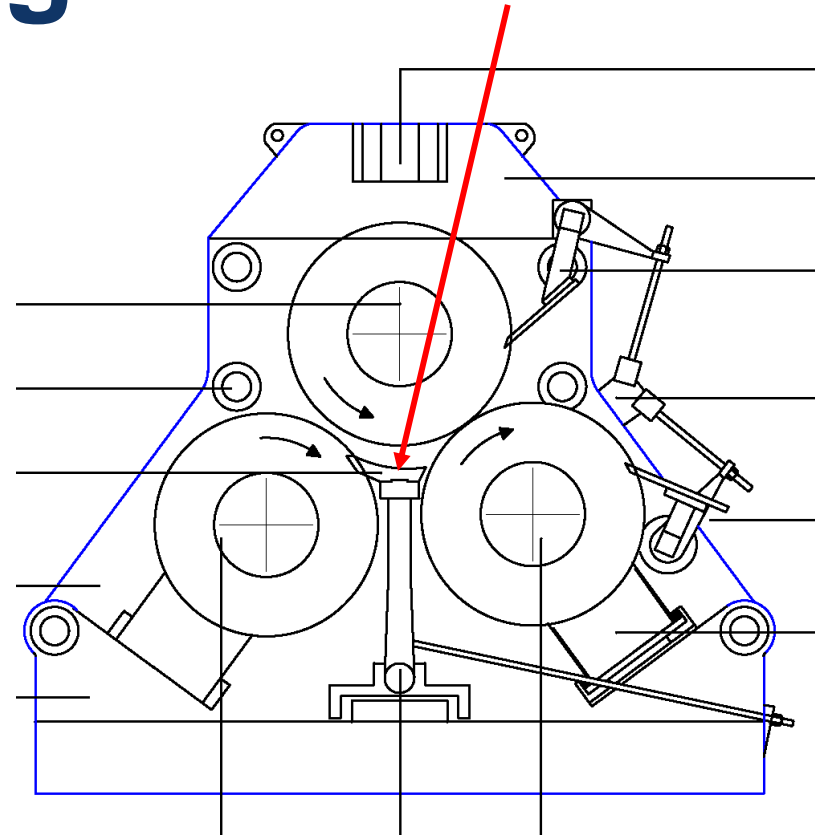
# Mill ratio

- Some Australian mills use reabsorption factor as a guide for adjusting settings
- High reabsorption factor
  - Reduce feed nip setting
- Low reabsorption factor
  - Reduce delivery nip setting

# Trash plate design and setting

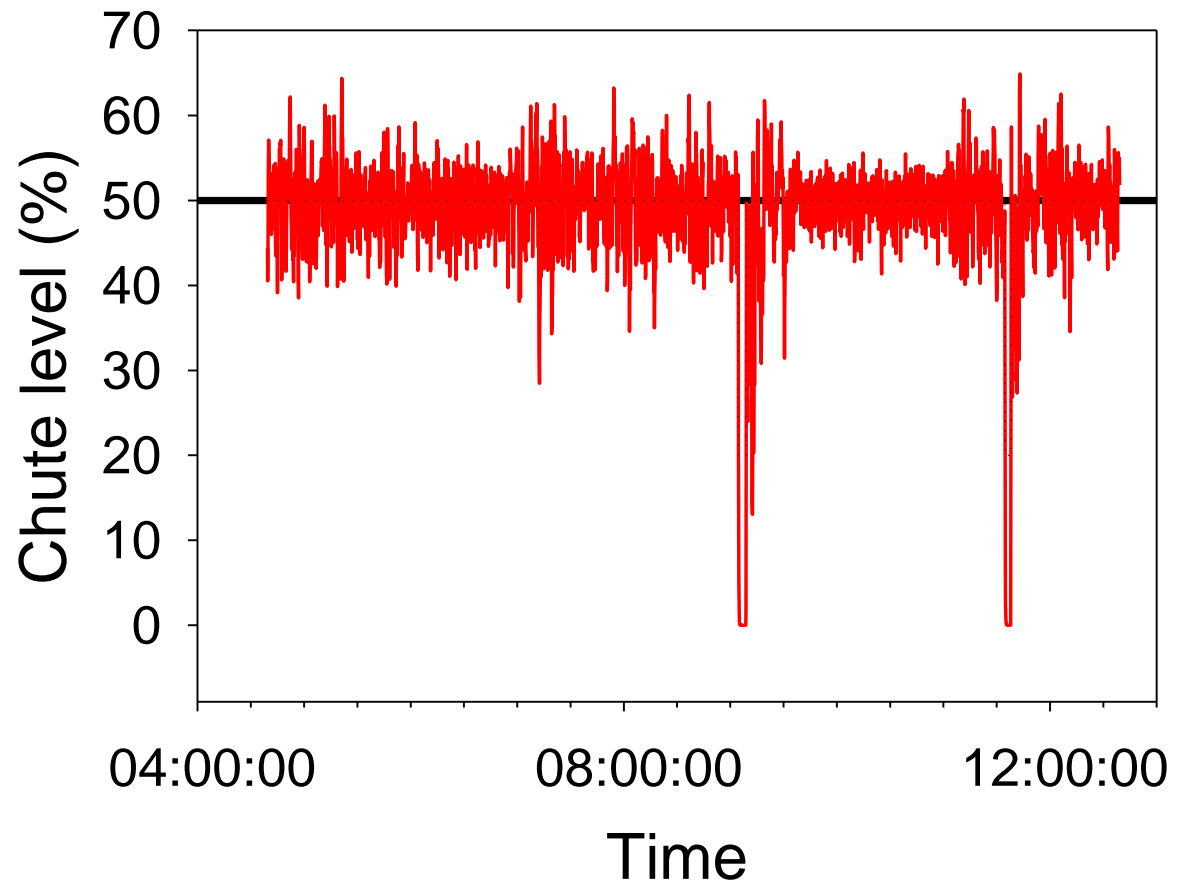
Trash plate

- Expect that trash plate design and setting will affect reabsorption factor
- No real evidence to suggest how
- Wide range of designs and settings that seem to function



# Mill control

- Good mill control can lead to lower reabsorption factors



# Power consumption



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# Reducing power consumption

- From roll load theory
$$R \propto LD(C_F - 0.1)$$
- $R$  Roll load
- $L$  Roll length
- $D$  Roll diameter
- $C_F$  Filling ratio (compaction)
- Power consumed between pairs of rolls
- Power consumed when pushing bagasse across plates

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# Reducing power consumption

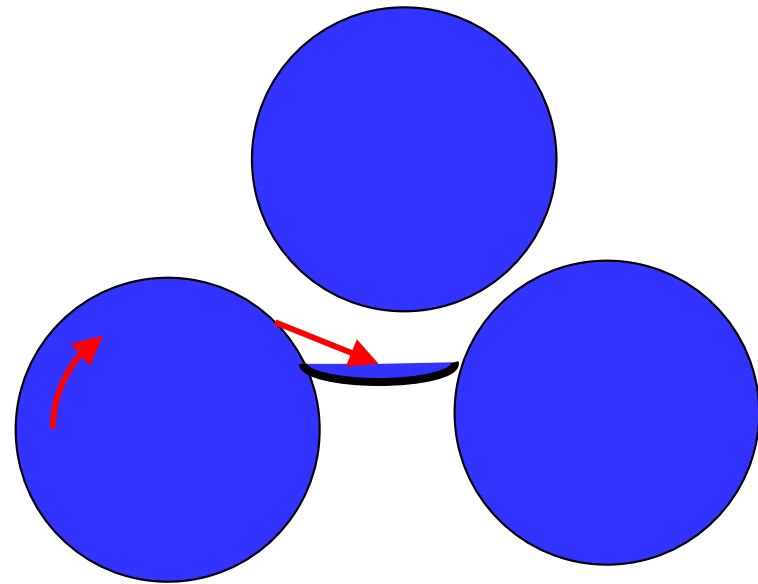
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- Power consumed between pairs of rolls
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# Power consumption in a four-roll mill

- Not much can be done to reduce power consumption in a four-roll mill without affecting performance
- Two-roll mill designs have the advantage of no trash plate
  - Generally lower capacity

# Trash plate effect

- From studies of mills with independent drives, torque on feed roll is of similar magnitude to torque on delivery roll, even though compaction is a lot lower
- Hypothesis that feed roll pushes bagasse across trash plate



# Power consumption innovations

- More efficient drives
  - Low efficiency steam turbines replaced by higher efficiency electric motors
    - Hydraulic transmissions
    - Variable speed drives and mechanical transmissions
- Independent drives
  - Pinionless mills



# Power consumption innovations

- More efficient mill couplings
- Rope couplings reported to reduce power consumption by 8% compared to tailbar couplings

